

## Sheared-flow modes in toroidal geometry

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Using a Fourier–Bessel representation for the fluctuating (turbulent) electrostatic potential, an equation governing the sheared-flow modes in toroidal geometry is derived from the gyrokinetic Poisson equation, where both the adiabatic and nonadiabatic responses of the electrons are taken into account. It is shown that the principal geometrical effect on sheared-flow modes of the electrostatic potential is due to the flux-surface average of  $1/B$ , where  $B$  is the magnetic field strength. © 2000 American Institute of Physics. [S1070-664X(00)00302-5]

### I. INTRODUCTION

It is now generally accepted in the fusion community that low-frequency, small-scale instabilities [e.g., drift waves, ion temperature gradient-driven (ITG) modes] are major contenders for the anomalous, cross-field transport<sup>1,2</sup> observed in tokamaks<sup>3</sup> and stellarators.<sup>4</sup> There is some experimental evidence<sup>5</sup> that (equilibrium) sheared flows (or zonal flows<sup>6</sup>) can have a strong impact on the turbulence-driven cross-field transport.<sup>7</sup> Therefore an accurate calculation of sheared-flow modes in toroidal geometry is an important issue.

In this paper, sheared-flow modes in toroidal geometry are calculated from the gyrokinetic Poisson's (GKP) equation.<sup>8</sup> A change of coordinate system allows us to write the fluctuating electrostatic potential in terms of Bessel–Fourier series. The case of a cylindrical plasma has been considered by Li, Lee, and Parker. In an unpublished report, these authors discuss the solution of the full GKP in cylindrical geometry with circular magnetic surfaces and no azimuthal magnetic field. By introducing a coordinate transformation, we extend the work of Li and co-workers to toroidal geometry; furthermore, the main goal of this paper is to consider the calculation of sheared-flow modes in toroidal geometry, rather than the solution of the (full) GKP in toroidal geometry, which requires a numerical approach.<sup>9</sup> It is shown that the principal geometrical effect on sheared-flow modes is due to the flux-surface average of the inverse of the magnetic field strength. The paper is organized as follows; in Sec. II, we introduce the gyrokinetic Poisson's equation; magnetic, toroidal (Shafranov-like) and cylindrical coordinate systems are discussed and the transformation between guiding center and particle coordinates are given in Sec. III, in the same section, the flux-surface average of the GKP equation is derived and an equation governing the sheared-flow modes in toroidal geometry is obtained; we conclude with some remarks in Sec. IV.

### II. GYRO-KINETIC POISSON EQUATION

Assuming that the Debye length is much smaller than the ion thermal gyroradius and neglecting electron gyroradius effects, the GKP equation can be written as<sup>8,10,11</sup>

$$\int d\mathbf{R}_{\text{gc}} \int d\mathbf{v} \left( F_i + \frac{e\tilde{\Phi}}{m_i B} \frac{\partial F_i}{\partial \mu} \right) \delta(\mathbf{R}_{\text{gc}} - \mathbf{r} + \boldsymbol{\rho}) = n_e, \quad (1)$$

where  $\tilde{\Phi} \equiv \Phi(\mathbf{r}) - \langle \Phi \rangle_{\text{gc}}(\mathbf{R}_{\text{gc}}, \mathbf{v})$ ,  $\mathbf{r} = \mathbf{R}_{\text{gc}} + \boldsymbol{\rho}$  is the particle position,  $\mathbf{R}_{\text{gc}}$  is the guiding center position,  $\langle \cdots \rangle_{\text{gc}}$  denotes a gyrophase average keeping the guiding center position fixed,  $\boldsymbol{\rho} \equiv \hat{\mathbf{e}}_{\parallel} \times \mathbf{v} / \omega_c$  is the ion gyroradius,  $\hat{\mathbf{e}}_{\parallel} \equiv \mathbf{B} / B$  is the unit vector along the confining magnetic field,  $\omega_c$  is the ion cyclotron frequency,  $\mu = v_{\perp}^2 / (2B)$  is the magnetic moment,  $F_i$  is the (total) ion guiding center distribution and  $n_e$  is the electron density. The aim of this paper is to calculate the flux-surface-averaged component of the electrostatic potential,  $\langle \Phi \rangle_S$ , from the GKP equation (1) in toroidal geometry. The operation  $\int d\mathbf{R}_{\text{gc}} [\cdots] \delta(\mathbf{R}_{\text{gc}} - \mathbf{r} + \boldsymbol{\rho})$  acts to transform the guiding center variables  $\{\mathbf{R}_{\text{gc}}, \mathbf{v}\}$  to the particle variables  $\{\mathbf{r}, \mathbf{v}\}$ . Although  $F_i$ ,  $\langle \Phi \rangle_{\text{gc}}$ , and  $B$  are functions of the guiding center variables, the integrand in equation (1) also depends on the particle variable  $\{\mathbf{r}, \mathbf{v}\}$  through  $\Phi$ . We write the ion distribution function as  $F_i = F_{i0}$  (equilibrium) +  $\delta F_i$  (fluctuation) and assume that the equilibrium part of  $F_i$  is Maxwellian

$$F_{i0} = \frac{n_0(\mathbf{R}_{\text{gc}})}{2\pi v_{\text{thi}}^2} \exp(-\mu B / v_{\text{thi}}^2) f(\mathbf{R}_{\text{gc}}, v_{\parallel}), \quad (2)$$

where  $v_{\text{thi}} \equiv (T_{i0}(\mathbf{R}_{\text{gc}}) / m_i)^{1/2}$  is the ion thermal velocity and  $f$  satisfies the normalization condition  $\int_{-\infty}^{+\infty} d v_{\parallel} f(\mathbf{R}_{\text{gc}}, v_{\parallel}) = 1$ . The volume element in velocity space is defined as  $d^3\mathbf{v} \equiv 2\pi v_{\perp} d v_{\perp} d v_{\parallel}$ . Assuming that  $|\partial \delta F_i / \partial \mu| \ll |\partial F_{i0} / \partial \mu|$  and using  $F_{i0}(\mathbf{R}_{\text{gc}}) \approx F_{i0}(\mathbf{r})$  and  $T_{i0}(\mathbf{R}_{\text{gc}}) \approx T_{i0}(\mathbf{r})$ , carrying out the integration over  $v_{\parallel}$  in Eq. (1), the GKP equation becomes

$$\int_0^{\infty} \langle \tilde{\Phi} \rangle_{\text{part}} V_{\perp} \exp(-V_{\perp}^2 / 2) dV_{\perp} = \frac{T_{i0}(\mathbf{r})}{e n_0(\mathbf{r})} (\bar{n}_i - n_e), \quad (3)$$

where  $V_{\perp} \equiv v_{\perp} / v_{\text{thi}}$  is the normalized perpendicular velocity,  $\langle \cdots \rangle_{\text{part}}$  denotes a gyrophase angle keeping the particle position fixed and

$$\bar{n}_i \equiv \int d\mathbf{R}_{\text{gc}} \int d\mathbf{v} F_i(\mathbf{R}_{\text{gc}}, \mathbf{v}) \delta(\mathbf{R}_{\text{gc}} - \mathbf{r} + \boldsymbol{\rho}) \quad (4)$$

can be calculated numerically by keeping the guiding center position fixed. The electron density can be written as  $n_e = n_e^{(A)} + n_e^{(\text{NA})}$ , where  $n_e^{(A)}$  and  $n_e^{(\text{NA})}$  are, respectively, the adiabatic and nonadiabatic parts of the electron density. The adiabatic response is of the form  $n_e^{(A)} \propto \Phi - \langle \Phi \rangle_S$ , where

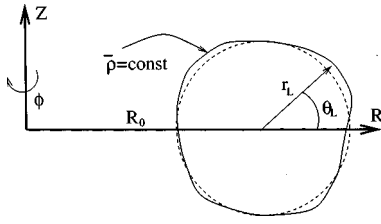


FIG. 1. Cylindrical coordinate system  $(R, Z, \phi)$  and local toroidal coordinate system  $(r_L, \theta_L, \phi_L = \phi)$  in toroidal geometry. A magnetic surface  $\bar{\rho} = \text{const}$  (plain line) and a tokamak-like magnetic surface (dotted line) are shown.

$\langle \dots \rangle_S$  denotes an average over the magnetic surface (see next section).

### III. MAGNETIC AND TOROIDAL COORDINATES

We consider a fully three-dimensional configuration with closed, nested magnetic surfaces. The confining magnetic field  $\mathbf{B}$  is written in straight-field line coordinates  $\{\bar{\rho}, \bar{\theta}, \bar{\zeta}\}$  as

$$\mathbf{B} = \nabla \alpha \times \nabla \Psi, \quad (5)$$

where  $\alpha \equiv \bar{\zeta} - q\bar{\theta}$  is the field line label,  $2\pi\Psi$  is the enclosed poloidal flux,  $\bar{\theta}$  is the magnetic poloidal angle and  $\bar{\zeta}$  is the magnetic toroidal angle. The radial label is denoted  $\bar{\rho}$  and, by definition,  $\mathbf{B} \cdot \nabla \bar{\rho} = 0$ . There is some freedom in specifying the radial label; here, for convenience, we define  $\bar{\rho} \equiv \sqrt{\psi_T / \psi_T^{(b)}}$ , where  $\psi_T$  is the toroidal flux enclosed within the magnetic surface, and  $\psi_T^{(b)}$  is  $\psi_T$  evaluated at the plasma boundary. By construction the radial label runs from 0 (magnetic axis) to 1 (last closed magnetic surface). The magnetic surfaces can be specified in cylindrical coordinates; for instance, in the equilibrium code VMEC<sup>12,13</sup> an expansion in Fourier series is used

$$\begin{aligned} R_l &= R_l(\bar{\rho}, \bar{\theta}, \bar{\zeta}) = \sum_{M=0}^{M_{\max}} \sum_{N=-N_{\max}}^{+N_{\max}} R_{MN} \cos(\Theta_{MN}), \\ Z_l &= Z_l(\bar{\rho}, \bar{\theta}, \bar{\zeta}) = \sum_{M=0}^{M_{\max}} \sum_{N=-N_{\max}}^{+N_{\max}} Z_{mn} \sin(\Theta_{MN}), \\ \phi_l &= \phi_l(\bar{\rho}, \bar{\theta}, \bar{\zeta}) = \bar{\zeta} - \frac{2\pi}{N_{\text{per}}} \sum_{M=0}^{M_{\max}} \sum_{N=-N_{\max}}^{+N_{\max}} \tilde{\phi}_{MN} \sin(\Theta_{MN}), \end{aligned} \quad (6)$$

where  $\Theta_{MN} \equiv M\bar{\theta} + N_{\text{per}}N\bar{\zeta}$  and  $N_{\text{per}}$  is the number of field periods of the configuration. For intermediate analytical calculations, it is convenient to work with the local toroidal coordinate system  $\{r_L, \theta_L, \phi_L\}$  shown in Fig. 1. In the plane  $\phi_L = \text{const}$ , the cylindrical radius  $R_L$  and the height  $Z_L$  are

$$\begin{aligned} R_L &= R_0 + r_L \cos \theta_L, \\ Z_L &= r_L \sin \theta_L. \end{aligned} \quad (7)$$

Here  $R_0$  is the average radius of the magnetic axis defined as

$$R_0 \equiv \frac{1}{4\pi^2} \int_0^{2\pi} d\bar{\theta} \int_0^{2\pi} d\bar{\zeta} R_L(\bar{\rho}=0, \bar{\theta}, \bar{\zeta}). \quad (8)$$

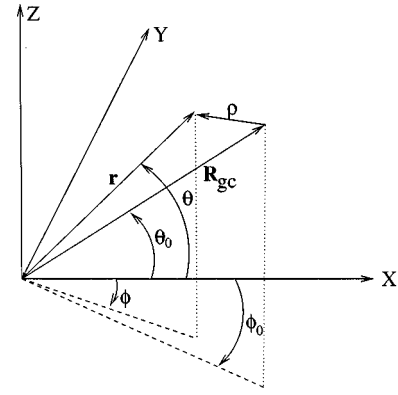


FIG. 2. Using the local coordinate system (Fig. 1), the particle position,  $\mathbf{r}$ , and its guiding center position,  $\mathbf{R}_{\text{gc}}$  can be labeled by  $(r, \theta, \phi)$  and  $(R_{\text{gc}}, \theta_0, \phi_0)$ , respectively. Here  $r \equiv (\mathbf{r} \cdot \mathbf{r})^{1/2}$  and  $R_{\text{gc}} \equiv (\mathbf{R}_{\text{gc}} \cdot \mathbf{R}_{\text{gc}})^{1/2}$ .

This definition is convenient for configurations with helical magnetic axis (e.g., heliac-type configurations). The curve  $r_L = \text{const}$  describes a circle in the plane  $\phi = \text{const}$ . Note that in general  $\nabla \bar{\rho} \times \nabla r_L \neq 0$ , so that  $\mathbf{B} \cdot \nabla r_L \neq 0$  along the  $r_L = \text{const}$  curve. Using Eqs. (6), one can invert Eqs. (7) to get

$$\tan \theta_L(\bar{\rho}, \bar{\theta}, \bar{\zeta}) = \frac{Z_L(\bar{\rho}, \bar{\theta}, \bar{\zeta})}{R_L(\bar{\rho}, \bar{\theta}, \bar{\zeta}) - R_0} \quad (9)$$

and

$$r_L(\bar{\rho}, \bar{\theta}, \bar{\zeta}) = \left[ [R_L(\bar{\rho}, \bar{\theta}, \bar{\zeta}) - R_0]^2 + Z_L^2(\bar{\rho}, \bar{\theta}, \bar{\zeta}) \right]^{1/2}, \quad (10)$$

where the explicit dependence on the magnetic coordinates  $\{\bar{\rho}, \bar{\theta}, \bar{\zeta}\}$  is shown. Although the inverse transformations (9) and (10) are exact, the fact that, in general,  $\nabla \bar{\rho} \times \nabla r_L \neq 0$ , complicates the representation of the fluctuating electrostatic potential  $\Phi$  in the gyrokinetic Poisson equation. As we shall see below, it is convenient to introduce a flux surface averaged toroidal system  $\{r, \theta, \phi\}$ . The radial label is defined as  $r \equiv \langle r_L(\bar{\rho}, \bar{\theta}, \bar{\zeta}) \rangle_S / a$  where  $a \equiv \langle r_L(\bar{\rho}=1, \bar{\theta}, \bar{\zeta}) \rangle_S$  and  $\langle \dots \rangle_S$  denotes an average over the magnetic surface. For an arbitrary function  $F$ ,  $\langle F \rangle_S$  is defined as

$$\langle F \rangle_S(\bar{\rho}) \equiv \frac{1}{A(\bar{\rho})} \int_0^{2\pi} d\bar{\zeta} \int_0^{2\pi} d\bar{\theta} \mathcal{J}(\bar{\rho}, \bar{\theta}, \bar{\zeta}) F(\bar{\rho}, \bar{\theta}, \bar{\zeta}), \quad (11)$$

where  $\mathcal{J} \equiv [\nabla \bar{\rho} \cdot (\nabla \bar{\theta} \times \nabla \bar{\zeta})]^{-1}$  is the Jacobian of the transformation and

$$A \equiv \int_0^{2\pi} d\bar{\zeta} \int_0^{2\pi} d\bar{\theta} \mathcal{J}(\bar{\rho}, \bar{\theta}, \bar{\zeta}) \quad (12)$$

is the area of the magnetic surface  $\bar{\rho} = \text{const}$ . For a configuration with a single magnetic axis, the relation  $r = r(\bar{\rho})$  is monotonous in  $\bar{\rho}$  and it can be easily inverted. Then we may write the fluctuating electrostatic potential as

$$\Phi = \sum_{l=1}^{\infty} \sum_{m, n=-\infty}^{\infty} \Phi_{lmn} J_m(\beta_{ml} r) \exp[i(m\theta + n\phi)], \quad (13)$$

where  $\beta_{ml}$  is the  $l$ th zero of the Bessel function of order  $m$ . We note that, locally,  $\theta$  and  $\phi$  in the above equation are

dependent on the magnetic coordinates  $\{\bar{\rho}, \bar{\theta}, \bar{\zeta}\}$ . Multiplying Eq. (13) by  $rJ_m(\beta_{ml}r)\exp(-im\theta-in\phi)$  and integrating over  $r$ ,  $\theta$  and  $\phi$  yields the coefficients  $\Phi_{lmn}$

$$\Phi_{lmn} = \frac{1}{2\pi^2 J_{m+1}^2(\beta_{ml})} \int_0^1 dr \int_0^{2\pi} d\theta \int_0^{2\pi} r J_m(\beta_{ml}r) \times \exp(-im\theta-in\phi) \Phi(r, \theta, \phi) d\phi, \quad (14)$$

where we have used the relation of orthogonality<sup>14</sup> of Bessel functions

$$\int_0^1 x J_N(\alpha x) J_N(\beta x) dx = \frac{\delta(\alpha-\beta)}{2} [J_{N+1}(\alpha)]^2. \quad (15)$$

The difficulty in calculating the flux-surface average of the GKP equation (1) arises in the  $\langle\langle\Phi\rangle_{\text{gc}}\rangle_{\text{part}}$  term. In particular we must transform back and forth between particle and guiding center variables; it is then convenient to use the cylindrical coordinates  $\{R, Z, \phi\}$  and the local toroidal coordinates  $\{r, \theta, \phi\}$  (right-handed in that order). It is easy to show the unit vectors in the local toroidal coordinates can be written as

$$\begin{aligned} \hat{\mathbf{r}} &= \cos\theta\hat{\mathbf{R}} + \sin\theta\hat{\mathbf{Z}} \\ &= +\cos\theta\cos\phi\hat{\mathbf{x}} - \cos\theta\sin\phi\hat{\mathbf{y}} + \sin\theta\hat{\mathbf{z}}, \\ \hat{\theta} &= \cos\theta\hat{\mathbf{Z}} - \sin\theta\hat{\mathbf{R}} \\ &= -\sin\theta\cos\phi\hat{\mathbf{x}} + \sin\theta\sin\phi\hat{\mathbf{y}} + \cos\theta\hat{\mathbf{z}}, \\ \hat{\phi} &= -\sin\phi\hat{\mathbf{x}} - \cos\phi\hat{\mathbf{y}}. \end{aligned} \quad (16)$$

Then one can use the set  $(r_0, \theta_0, \phi_0)$  to label the guiding center position, and the particle position  $\mathbf{r}(r, \theta, \phi) = \mathbf{R}_{\text{gc}}(r_0, \theta_0, \phi_0) + \boldsymbol{\rho}$  can also be written as (Fig. 2)

$$R_0\hat{\mathbf{R}} + r\hat{\mathbf{r}} = R_0\hat{\mathbf{R}}_{\text{gc}} + r_0\hat{\mathbf{r}}_0 + \boldsymbol{\rho}, \quad (17)$$

where  $\hat{\mathbf{R}}_{\text{gc}} \equiv \cos\phi_0\hat{\mathbf{x}} - \sin\phi_0\hat{\mathbf{y}}$ . Noting that the particle velocity can be written as (Fig. 3)

$$\mathbf{v} = v_{\parallel}\hat{\mathbf{e}}_{\parallel} + v_{\perp}(\cos\varphi\hat{\mathbf{n}} + \sin\varphi\hat{\mathbf{b}}), \quad (18)$$

where  $\hat{\mathbf{n}} \equiv [\nabla\Psi/(\nabla\Psi \cdot \nabla\Psi)^{1/2}]_{r_0, \theta_0, \xi_0}$  is the unit normal vector,  $\hat{\mathbf{e}}_{\parallel} \equiv \mathbf{B}/B$  is the unit vector along  $\mathbf{B}$ ,  $\hat{\mathbf{b}} \equiv [\hat{\mathbf{e}}_{\parallel} \times \hat{\mathbf{n}}]_{r_0, \theta_0, \xi_0}$  is the unit binormal vector, and  $\varphi$  is the gyroangle, the components of Eq. (17) yield [neglecting corrections  $\mathcal{O}(\rho^2/R_0^2)$  and higher]

$$\Delta\phi \approx \frac{\boldsymbol{\rho} \cdot \hat{\boldsymbol{\phi}}_0}{R}, \quad (19)$$

where, as before,  $R = R_0 + r\cos\theta$  is the cylindrical radius; and

$$\begin{aligned} r\cos\Delta\theta - \rho''\cos\psi'' &= r_0, \\ r\sin\Delta\theta - \rho''\sin\psi'' &= 0, \end{aligned} \quad (20)$$

where we have introduced the new variables  $\rho''$  and  $\psi''$  such that

$$\begin{aligned} \rho''\sin\psi'' &= \rho\sin\psi(\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\theta}}_0) + \rho\cos\psi(\hat{\mathbf{n}} \cdot \hat{\boldsymbol{\theta}}_0), \\ \rho''\cos\psi'' &= \rho\cos\psi(\hat{\mathbf{n}} \cdot \hat{\mathbf{r}}_0) + \rho\sin\psi(\hat{\mathbf{b}} \cdot \hat{\mathbf{r}}_0), \end{aligned} \quad (21)$$

and  $\psi \equiv \varphi - 3\pi/2$ . Using the Fourier–Bessel representation (13) and taking into account Eqs. (19), (20), and (21) one can show that (Appendix A)

$$\begin{aligned} \langle\langle\Phi\rangle_{\text{gc}}\rangle_{\text{part}} &= \sum_{l=1}^{\infty} \sum_{m,n=-\infty}^{\infty} \Phi_{lmn} \exp(im\theta+in\phi) \left\{ \sum_{k=-\infty}^{\infty} (-1)^k J_k(\beta_{ml}\rho'') J_k(k_t\rho'') J_{m+k}(\beta_{ml}r) J_0(\hat{k}\rho'') \right. \\ &\quad \left. + \frac{\beta_{ml}}{4} \rho'' \sum_{k=-\infty}^{\infty} (-1)^k J_k(\beta_{ml}\rho'') J_k(k_t\rho'') [J_{m+k+1}(\beta_{ml}r) - J_{m+k-1}(\beta_{ml}r)] [J_1(x_+) - J_1(x_-)] \right\}. \end{aligned} \quad (22)$$

Here  $k_t \equiv ng/R$ , where  $g \equiv (\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\phi}}_0)/(\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\phi}}_0)$ , is the toroidal wave number;  $k_p \equiv m/r$  is the poloidal wave number;  $\hat{k} \equiv k_p + k_t$  and  $x_{\pm} \equiv (\hat{k} \pm 1/r)\rho''$ . In the limit  $B_{\theta} \rightarrow 0$ , it can be shown (Appendix B) that Eq. (22) reduces to

$$\begin{aligned} \langle\langle\Phi\rangle_{\text{gc}}\rangle_{\text{part}} &= \sum_{l=1}^{\infty} \sum_{m,n=-\infty}^{\infty} \Phi_{lmn} \exp(im\theta+in\phi) \\ &\quad \times J_m(\beta_{ml}r) J_0^2(\beta_{ml}\rho), \end{aligned} \quad (23)$$

which is the expression derived by Li *et al.* Unlike the cylindrical case, we note that  $\langle\langle\Phi\rangle_{\text{gc}}\rangle_{\text{part}}$  depends explicitly on the poloidal and toroidal wave numbers. Substituting  $\Phi$  [Eq. (13)] and  $\langle\langle\Phi\rangle_{\text{gc}}\rangle_{\text{part}}$  [Eq. (22)] in the GKP equation (3),

using the integral representation of the Bessel functions<sup>15</sup> and carrying out the integration over  $V_{\perp}$  yields (Appendix B)

$$\begin{aligned} \sum_{l=1}^{\infty} \Phi_{l00} \left\{ J_0(\beta_{0l}r) [1 - \exp(-C_l^2/2)] \right. \\ \left. + \frac{\langle\rho_i\rangle_S/r}{\Gamma(2)} J_1(\beta_{0l}r) C_l \left( 1 - \frac{C_l^2}{2} \right) \exp(-C_l^2/2) \right\} = \mathcal{D}(r), \end{aligned} \quad (24)$$

where  $C_l \equiv \beta_{0l}\langle\rho_i\rangle_S$ ; here  $\langle\rho_i\rangle_S$  is the flux surface average of the ion thermal gyroradius and the right-hand side,  $\mathcal{D}(r) \equiv T_{i0}[\langle n_i \rangle_S - \langle n_e^{(\text{NA})} \rangle_S]/(en_0)$ , can be evaluated numerically. In deriving the expression for  $\mathcal{D}(r)$  we have taken into account the fact that  $n_e^{(\text{A})} \propto \Phi - \langle\Phi\rangle_S$  so that  $\langle n_e^{(\text{A})} \rangle_S \equiv 0$ . In Eq.

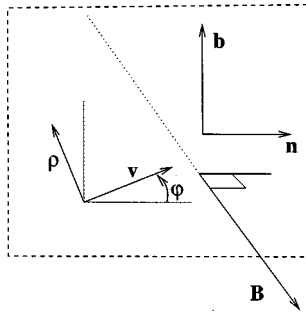


FIG. 3. The perpendicular component of the particle velocity can be written as  $\mathbf{v}_\perp = v_\perp (\cos \varphi \hat{\mathbf{n}} + \sin \varphi \hat{\mathbf{b}})$ , where  $\hat{\mathbf{n}}$  is normal to the magnetic surface, and  $\hat{\mathbf{b}} \propto \mathbf{B} \times \hat{\mathbf{n}}$  is the binormal vector. The gyroradius vector,  $\boldsymbol{\rho}$ , is defined as  $\boldsymbol{\rho} \equiv (\mathbf{B}/B) \times \mathbf{v}/\omega_c$  where  $\omega_c$  is the cyclotron frequency.

(24), corrections  $\mathcal{O}[\langle \rho_i \rangle_S / r]^2 \ll 1$  and higher have been neglected. Since  $\langle \rho_i \rangle_S \propto \langle 1/B \rangle_S$ , it is clear from Eq. (24) that the principal geometrical effect on sheared-flow modes is due to the flux-surface average of  $1/B$ . However, this geometrical dependence is nonlinear. Finally it is worth pointing out that the coefficients of  $\Phi_{l00}$  tend asymptotically towards zero as  $C_l \rightarrow 0$ , as it should be; the limit  $C_l \rightarrow 0$  (which is the counterpart of  $k_\perp \rho_l \rightarrow 0$  in slab geometry) correspond to modes that cannot have a radial structure. If higher-order corrections were to be taken into account, the coupling between the  $\Phi_{l\pm 10}$  modes and flux-surface averaged equilibrium quantities should be retained in Eq. (24). Therefore the calculation of sheared-flow modes in low-aspect-ratio configurations (e.g., spherical tokamaks) would require a different approach than presented in this paper.

There are various mechanisms that can excite sheared-flow modes in toroidal geometry. For instance, it has been shown by Diamond and Kim that the poloidal flow in a toroidal plasma can be accelerated when there is a gradient in the turbulent Reynolds stress.<sup>16</sup> As shown by Diamond *et al.*,<sup>6</sup> zonal flows can be generated by modulational instability of a drift-wave turbulence and, in turn, regulate the turbulence. Furthermore any mechanism that can influence the fraction of non-adiabatic electrons can also modify the sheared-flow modes, through a modification of the source term on the right-hand side of Eq. (24); the relative importance of the nonadiabatic electrons is of course model dependent.

#### IV. CONCLUDING REMARKS

In this paper, an equation governing sheared-flow modes in toroidal geometry has been derived. By introducing a local system of Shafranov-type toroidal coordinates and by using a Fourier–Bessel representation (which exploits the toroidicity of the configuration) for the electrostatic potential, the flux-surface average of the gyrokinetic Poisson has been obtained. It has been shown that the principal geometrical effect on sheared-flow modes is due to  $\langle 1/B \rangle_S$ , where  $\langle \cdots \rangle_S$ . The equation for sheared-flow modes (24) can be solved numerically by quadrature.

#### APPENDIX A: GYRO-PHASE-AVERAGED ELECTROSTATIC POTENTIAL IN TOROIDAL GEOMETRY

The basic coordinate systems used in this appendix are the cylindrical coordinates  $\{R, Z, \phi\}$  and the local toroidal coordinates  $\{r, \theta, \phi\}$ . The unit vectors in cylindrical coordinates can be decomposed onto a local Cartesian system:  $\hat{\mathbf{R}} = \cos \phi \hat{\mathbf{x}} - \sin \phi \hat{\mathbf{y}}$ ,  $\hat{\phi} = -\sin \phi \hat{\mathbf{x}} - \cos \phi \hat{\mathbf{y}}$  and  $\hat{\mathbf{Z}} = \hat{\mathbf{z}}$ . The unit vectors in the local toroidal coordinate system  $\{r, \theta, \phi\}$  can now be determined; since  $\hat{\mathbf{r}}$  and  $\hat{\phi}$  are orthogonal, we note that  $\hat{\mathbf{r}} = (\hat{\mathbf{r}} \cdot \hat{\mathbf{R}}) \hat{\mathbf{R}} + (\hat{\mathbf{r}} \cdot \hat{\mathbf{Z}}) \hat{\mathbf{Z}}$  and  $\hat{\theta} = \hat{\phi} \times \hat{\mathbf{r}}$  so that  $\hat{\mathbf{r}} = \cos \theta \hat{\mathbf{R}} + \sin \theta \hat{\mathbf{Z}}$  and  $\hat{\theta} = \cos \theta \hat{\mathbf{Z}} - \sin \theta \hat{\mathbf{R}}$ . In explicit form, we have

$$\begin{aligned} \hat{\mathbf{r}} &= +\cos \theta \cos \phi \hat{\mathbf{x}} - \cos \theta \sin \phi \hat{\mathbf{y}} + \sin \theta \hat{\mathbf{z}}, \\ \hat{\theta} &= -\sin \theta \cos \phi \hat{\mathbf{x}} + \sin \theta \sin \phi \hat{\mathbf{y}} + \cos \theta \hat{\mathbf{z}}, \\ \hat{\phi} &= -\sin \phi \hat{\mathbf{x}} - \cos \phi \hat{\mathbf{y}}. \end{aligned} \quad (\text{A1})$$

The particle position vector,  $\mathbf{r}$ , can be written as  $\mathbf{r} = \mathbf{R}_{\text{gc}} + \boldsymbol{\rho}$ , where  $\mathbf{R}_{\text{gc}} = \mathbf{R}_{\text{gc}}(r_0, \theta_0, \phi_0)$  is the position of the guiding center and  $\boldsymbol{\rho} = \hat{\mathbf{e}}_\parallel \times \mathbf{v}/\omega_c$  is the gyroradius vector; here  $\hat{\mathbf{e}}_\parallel \equiv \mathbf{B}/B$  is the unit vector along  $\mathbf{B}$ . The local unit vectors associated with  $\mathbf{R}_{\text{gc}}$  are similar to Eq. (A1) with the replacement  $\theta \rightarrow \theta_0$  and  $\phi \rightarrow \phi_0$ . Then we obtain

$$\begin{aligned} \hat{\mathbf{r}} &= (\cos \theta \cos \theta_0 \cos \Delta \phi + \sin \theta \sin \theta_0) \hat{\mathbf{r}}_0 \\ &\quad + (\sin \theta \cos \theta_0 - \cos \theta \sin \theta_0 \cos \Delta \phi) \hat{\theta}_0 \\ &\quad + \cos \theta \sin \Delta \phi \hat{\phi}_0, \\ \hat{\theta} &= (\cos \theta \sin \theta_0 - \sin \theta \cos \theta_0 \cos \Delta \phi) \hat{\mathbf{r}} \\ &\quad + (\cos \theta \cos \theta_0 + \sin \theta \sin \theta_0 \cos \Delta \phi) \hat{\theta}_0 \\ &\quad - \sin \theta \sin \Delta \phi \hat{\phi}_0, \\ \hat{\phi} &= -\cos \theta_0 \sin \Delta \phi \hat{\mathbf{r}}_0 + \sin \theta_0 \sin \Delta \phi \hat{\theta}_0 + \cos \Delta \phi \hat{\phi}_0, \end{aligned} \quad (\text{A2})$$

where  $\Delta \phi \equiv \phi - \phi_0$ . The particle velocity can be written as  $\mathbf{v} = v_\parallel \hat{\mathbf{e}}_\parallel + v_\perp (\cos \varphi \hat{\mathbf{n}} + \sin \varphi \hat{\mathbf{b}})$ , where  $\hat{\mathbf{n}} \equiv [\nabla \Psi / (\nabla \Psi \cdot \nabla \Psi)^{1/2}]_{r_0, \theta_0, \phi_0}$  is the unit normal vector,  $\hat{\mathbf{e}}_\parallel \equiv \mathbf{B}/B$  is the unit vector along  $\mathbf{B}$ ,  $\hat{\mathbf{b}} \equiv [\hat{\mathbf{e}}_\parallel \times \hat{\mathbf{n}}]_{r_0, \theta_0, \phi_0}$  is the unit binormal vector, and  $\varphi$  is the gyroangle (Fig. 2). Then we may write the gyroradius vector as  $\boldsymbol{\rho} = \omega_c^{-1} (\hat{\mathbf{e}}_\parallel \times \mathbf{v}) = \rho (\cos \varphi \hat{\mathbf{b}} - \sin \varphi \hat{\mathbf{n}})$ , where  $\rho \equiv v_\perp / \omega_c$ . Without loss of generality, the relation  $\mathbf{r} = \mathbf{R}_{\text{gc}} + \boldsymbol{\rho}$  can be written as

$$R_0 \hat{\mathbf{R}} + r \hat{\mathbf{r}} = R_0 \hat{\mathbf{R}}_{\text{gc}} + r_0 \hat{\mathbf{r}}_0 + \boldsymbol{\rho}, \quad (\text{A3})$$

where  $\hat{\mathbf{R}}_{\text{gc}} \equiv \cos \phi_0 \hat{\mathbf{x}} - \sin \phi_0 \hat{\mathbf{y}}$ . Taking the scalar product of Eq. (A3) with  $\hat{\mathbf{r}}_0$ ,  $\hat{\theta}_0$  and  $\hat{\phi}_0$ , noting that  $\hat{\mathbf{R}}_{\text{gc}} \cdot \hat{\phi}_0 = \hat{\mathbf{r}}_0 \cdot \hat{\phi}_0 = 0$ ,  $\hat{\mathbf{R}} \cdot \hat{\phi}_0 = \cos \theta \hat{\mathbf{r}} \cdot \hat{\phi}_0 - \sin \theta \hat{\theta} \cdot \hat{\phi}_0 = \sin \Delta \phi$ ,  $\hat{\mathbf{R}} \cdot \hat{\mathbf{r}}_0 = \cos \theta \hat{\mathbf{r}} \cdot \hat{\mathbf{r}}_0 - \sin \theta \hat{\theta} \cdot \hat{\mathbf{r}}_0 = \cos \theta_0 \cos \Delta \phi$ ,  $\hat{\mathbf{R}} \cdot \hat{\theta}_0 = \cos \theta \hat{\mathbf{r}} \cdot \hat{\theta}_0 - \sin \theta \hat{\theta} \cdot \hat{\theta}_0 = -\sin \theta_0 \cos \Delta \phi$ , neglecting corrections  $\mathcal{O}(\rho^2/R_0^2)$  and higher we get



$$\begin{aligned} \sin \Delta \phi &= \frac{\boldsymbol{\rho} \cdot \hat{\boldsymbol{\phi}}_0}{R}, \\ r \cos(\theta - \theta_0) - r_0 &= \boldsymbol{\rho} \cdot \hat{\mathbf{r}}_0, \\ r \sin(\theta - \theta_0) &= \boldsymbol{\rho} \cdot \hat{\boldsymbol{\theta}}_0. \end{aligned} \tag{A4}$$

The geometrical effects are contained in the  $\boldsymbol{\rho} \cdot \hat{\mathbf{r}}_0$ ,  $\boldsymbol{\rho} \cdot \hat{\boldsymbol{\theta}}_0$ , and  $\boldsymbol{\rho} \cdot \hat{\boldsymbol{\phi}}_0$  terms. Introducing a new gyroangle  $\psi \equiv \varphi - 3\pi/2$ , we obtain the following set of equations

$$\begin{aligned} r \cos \Delta \theta - \rho \cos \psi(\hat{\mathbf{n}} \cdot \hat{\mathbf{r}}_0) &= r_0 + \rho \sin \psi(\hat{\mathbf{b}} \cdot \hat{\mathbf{r}}_0), \\ r \sin \Delta \theta - \rho \sin \psi(\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\theta}}_0) &= \rho \cos \psi(\hat{\mathbf{n}} \cdot \hat{\boldsymbol{\theta}}_0). \end{aligned} \tag{A5}$$

It is convenient to introduce new variables  $\rho''$  and  $\psi''$  such that

$$\begin{aligned} \rho'' \sin \psi'' &= \rho \sin \psi(\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\theta}}_0) + \rho \cos \psi(\hat{\mathbf{n}} \cdot \hat{\boldsymbol{\theta}}_0), \\ \rho'' \cos \psi'' &= \rho \cos \psi(\hat{\mathbf{n}} \cdot \hat{\mathbf{r}}_0) + \rho \sin \psi(\hat{\mathbf{b}} \cdot \hat{\mathbf{r}}_0). \end{aligned} \tag{A6}$$

Then we may rewrite Eqs. (A5) in a simpler form

$$\begin{aligned} r \cos \Delta \theta - \rho'' \cos \psi'' &= r_0, \\ r \sin \Delta \theta - \rho'' \sin \psi'' &= 0. \end{aligned} \tag{A7}$$

Using (A4) and  $\psi = \varphi - 3\pi/2$ , we note that  $\Delta \phi \approx \rho[\cos \psi(\hat{\mathbf{n}} \cdot \hat{\boldsymbol{\phi}}_0) + \sin \psi(\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\phi}}_0)]/R$ ; in a tokamak with  $B_\theta \ll B_\phi$ , one gets  $\hat{\mathbf{b}} \rightarrow \hat{\boldsymbol{\theta}}_0$  so that  $\Delta \phi \rightarrow 0$  and the problem is essentially two-dimensional. To leading order, one can show that

$$\begin{aligned} \Delta \theta &\approx \frac{\rho''}{r_0} \sin \psi'', \\ \Delta \phi &\approx f \frac{\rho''}{R} \cos \psi'' + g \frac{\rho''}{R} \sin \psi'', \end{aligned} \tag{A8}$$

where

$$f \equiv \frac{\hat{\mathbf{n}} \cdot \hat{\boldsymbol{\phi}}_0}{\hat{\mathbf{n}} \cdot \hat{\mathbf{r}}_0} \quad \text{and} \quad g \equiv \frac{\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\phi}}_0}{\hat{\mathbf{b}} \cdot \hat{\boldsymbol{\theta}}_0}. \tag{A9}$$

In a low- $\beta$  tokamak plasma with circular magnetic surfaces,  $f=0$  and  $g \sim B_\theta/B_\phi = \mathcal{O}(\epsilon) \ll 1$ , where  $\epsilon$  is the inverse aspect ratio. It is easy to see that  $f$  is related to the noncircularity of the magnetic surfaces; in general, we expect  $f \ll g$  (at least in the average sense). In the complex plane, Eqs. (A7) can be written in compact form as

$$r \exp(i\theta) = \rho'' \exp(i\psi'' + i\theta_0) + r_0 \exp(i\theta_0). \tag{A10}$$

For an arbitrary function  $F$ , we define  $\langle F \rangle_{\text{gc}} = (2\pi)^{-1} \times \int_{-\pi}^{+\pi} F(r, \theta, \phi, \varphi) d\varphi$  (for fixed guiding center position) and  $\langle F \rangle_{\text{part}} = (2\pi)^{-1} \int_{-\pi}^{+\pi} F(r_0, \theta_0, \phi_0, \varphi) d\varphi$  (for fixed particle position). For fixed guiding center (fixed  $r_0, \theta_0, \phi_0$ ), one can use Graf's theorem<sup>14</sup>

$$J_N(w) \exp(iN\theta) = \sum_{k=-\infty}^{\infty} J_{N+k}(u) J_k(v) \exp(ik\alpha), \tag{A11}$$

where  $u, v, w$ , and  $\alpha$  satisfy  $w = (u^2 + v^2 - 2uv \cos \alpha)^{1/2}$ ,  $u - v \cos \alpha = w \cos \theta$ ,  $v \sin \alpha = w \sin \theta$ , to get

$$\begin{aligned} J_m(\beta_{ml}r) \exp[im(\theta - \theta_0)] \\ = \sum_{k=-\infty}^{\infty} J_{m+k}(\beta_{ml}r_0) J_k(\beta_{ml}\rho'') \exp[-ik(\pi + \psi'')]. \end{aligned} \tag{A12}$$

Similarly, for fixed particle position, Graf's theorem (A11) yields

$$\begin{aligned} J_m(\beta_{ml}r_0) \exp[im(\theta_0 - \theta)] \\ = \sum_{k=-\infty}^{\infty} J_{m+k}(\beta_{ml}r) J_k(\beta_{ml}\rho'') \exp[ik(\theta - \theta_0 - \psi'')], \end{aligned} \tag{A13}$$

We multiply Eq. (A12) by  $\exp(in\phi + im\theta_0) = \exp(in\phi_0 + im\theta_0) \exp(in\Delta\phi)$  and operate with  $\langle \dots \rangle_{\text{gc}}$  on the resulting equation

$$\begin{aligned} \langle J_m(\beta_{ml}r) \exp(im\theta + in\phi) \rangle_{\text{gc}} \\ = \exp(im\theta_0 + in\phi_0) \sum_{k=-\infty}^{\infty} J_{m+k}(\beta_{ml}r_0) J_k(\beta_{ml}\rho'') \\ \times \langle \exp(in\Delta\phi) \exp[-ik(\pi + \psi'')] \rangle_{\text{gc}}. \end{aligned} \tag{A14}$$

Taking into account  $|f| \ll |g|$ , we may write  $in\Delta\phi \approx k_t \rho'' \sin \psi''$ ; here  $k_t \equiv ng/R$  is the toroidal wavenumber where, as before,  $R = R_0 + r \cos \theta$  is the cylindrical radius. Then

$$\begin{aligned} \langle J_m(\beta_{ml}r) \exp(im\theta + in\phi) \rangle_{\text{gc}} \\ = \exp(im\theta_0 + in\phi_0) \sum_{k=-\infty}^{\infty} J_{m+k}(\beta_{ml}r_0) J_k(\beta_{ml}\rho'') \\ \times \exp(-ik\pi) \langle \exp(ik_t \rho'' \sin \psi'' - ik\psi'') \rangle_{\text{gc}} \\ = \exp(im\theta_0 + in\phi_0) \\ \times \sum_{k=-\infty}^{\infty} (-1)^k J_{m+k}(\beta_{ml}r_0) J_k(\beta_{ml}\rho'') J_k(k_t \rho'') \\ = \exp(im\theta + in\phi) \left[ \exp(-im\Delta\theta) \exp(-in\Delta\phi) \right. \\ \left. \times \sum_{k=-\infty}^{\infty} (-1)^k J_{m+k}(\beta_{ml}r_0) J_k(\beta_{ml}\rho'') J_k(k_t \rho'') \right], \end{aligned} \tag{A15}$$

where we used the integral representation for Bessel functions<sup>15</sup>

$$\begin{aligned} J_N(x) &= \frac{1}{\pi} \int_0^\pi \cos(x \sin \theta - N\theta) d\theta \\ &= \frac{i^{-N}}{\pi} \int_0^\pi \exp(ix \cos \theta) \cos(N\theta) d\theta. \end{aligned} \tag{A16}$$

Using the recurrence relation,<sup>15</sup>  $dJ_N/dx = [J_{N-1}(x) - J_{N+1}(x)]/2$  (for  $N$  integer), we may write and

$$J_{m+k}(\beta_{m1}r_0) = J_{m+k}(\beta_{m1}r) + \frac{\beta_{m1}}{2} \rho'' \cos \lambda [J_{m+k+1}(\beta_{m1}r) - J_{m+k-1}(\beta_{m1}r)] + \dots, \quad (\text{A17})$$

in Eq. (A15); operating with  $\langle \dots \rangle_{\text{part}}$  (keeping  $r$ ,  $\theta$ , and  $\phi$  constants) on the resulting equation, one gets

$$\begin{aligned} \langle \langle J_m(\beta_{m1}r) \exp(im\theta + in\phi) \rangle_{\text{gc}} \rangle_{\text{part}} &= \exp(im\theta + in\phi) \left\{ \sum_{k=-\infty}^{\infty} (-1)^k J_k(\beta_{m1}\rho'') J_k(k_t \rho'') \right. \\ &\quad \times J_{m+k}(\beta_{m1}r) \langle \exp(-im\Delta\theta - in\Delta\phi) \rangle_{\text{part}} + \frac{\beta_{m1}}{2} \rho'' \sum_{k=-\infty}^{\infty} (-1)^k J_k(\beta_{m1}\rho'') J_k(k_t \rho'') \\ &\quad \left. \times [J_{m+k+1}(\beta_{m1}r) - J_{m+k-1}(\beta_{m1}r)] \langle \cos \lambda \exp(-im\Delta\theta - in\Delta\phi) \rangle_{\text{part}} + \dots \right\}, \quad (\text{A18}) \end{aligned}$$

where  $\lambda = \Delta\theta - \psi''$  and  $m\Delta\theta \approx k_p \rho'' \sin \psi''$ , where  $k_p \equiv m/r$  is the poloidal wave number. Let  $\hat{k} \equiv k_p + k_t$  and use the integral representation (A16) to show that  $\langle \exp(-im\Delta\theta - in\Delta\phi) \rangle_{\text{part}} = J_0(\hat{k}\rho'')$ . Write  $\cos \lambda = [\exp(i\lambda) + \exp(-i\lambda)]/2$  to obtain

$$\begin{aligned} \langle \cos \lambda \exp(-im\Delta\theta - in\Delta\phi) \rangle_{\text{part}} &= \langle \exp(-ix_- \sin \psi'' - i\psi'') \rangle_{\text{part}}/2 \\ &\quad + \langle \exp(-ix_+ \sin \psi'' + i\psi'') \rangle_{\text{part}}/2 \\ &= [J_1(x_+) - J_1(x_-)]/2, \end{aligned}$$

where  $x_{\pm} \equiv (\hat{k} \pm 1/r)\rho''$ . Combining the above results we can write

$$\begin{aligned} \langle \langle J_m(\beta_{m1}r) \exp(im\theta + in\phi) \rangle_{\text{gc}} \rangle_{\text{part}} &= \exp(im\theta + in\phi) \left\{ \sum_{k=-\infty}^{\infty} (-1)^k J_k(\beta_{m1}\rho'') J_k(k_t \rho'') \right. \\ &\quad \times J_{m+k}(\beta_{m1}r) J_0(\hat{k}\rho'') + \frac{\beta_{m1}}{4} \rho'' \\ &\quad \times \sum_{k=-\infty}^{\infty} (-1)^k J_k(\beta_{m1}\rho'') J_k(k_t \rho'') [J_{m+k+1}(\beta_{m1}r) \\ &\quad \left. - J_{m+k-1}(\beta_{m1}r)] [J_1(x_+) - J_1(x_-)] \right\}. \quad (\text{A19}) \end{aligned}$$

For the case of a strong toroidal magnetic field, the above result [Eq. (A19)] can be considerably simplified. In the limit  $B_{\theta} \rightarrow 0$ , we note that  $\hat{\mathbf{e}}_{\parallel} = \mathbf{B}/B \mapsto \hat{\phi}_0$ ,  $\hat{\mathbf{b}} \mapsto \hat{\theta}_0$  and  $\Delta\phi = \phi - \phi_0 \mapsto 0$ . Using Eq. (A12), we have

$$\begin{aligned} \langle J_m(\beta_{m1}r) \exp(im\theta + in\phi) \rangle_{\text{gc}} &= \exp(im\theta_0 + in\phi) J_m(\beta_{m1}r_0) J_0(\beta_{m1}\rho''), \quad (\text{A20}) \end{aligned}$$

since  $\langle \exp[-ik(\pi + \psi'')] \rangle_{\text{gc}} = \delta(k)$ . Operating with  $\langle \dots \rangle_{\text{part}}$  on Eq. (A20) and using Eq. (A13), we get

$$\begin{aligned} \langle \langle J_m(\beta_{m1}r) \exp(im\theta + in\phi) \rangle_{\text{gc}} \rangle_{\text{part}} &= \exp(in\phi) \langle \exp(im\theta_0) J_m(\beta_{m1}r_0) \rangle_{\text{part}} J_0(\beta_{m1}\rho'') \\ &= \exp(im\theta + in\phi) \\ &\quad \times \left\langle \sum_{k=-\infty}^{\infty} J_{m+k}(\beta_{m1}r) J_k(\beta_{m1}\rho'') \right. \\ &\quad \left. \times \exp[ik(\theta - \theta_0 - \psi'')] \right\rangle_{\text{part}} J_0(\beta_{m1}\rho'') \\ &= \exp(im\theta + in\phi) \\ &\quad \times \sum_{k=-\infty}^{\infty} J_{m+k}(\beta_{m1}r) J_k(\beta_{m1}\rho'') J_0(\beta_{m1}\rho'') \\ &\quad \times \langle \exp[ik(\theta - \theta_0 - \psi'')] \rangle_{\text{part}} \\ &= \exp(im\theta + in\phi) J_m(\beta_{m1}r) J_0^2(\beta_{m1}\rho''), \quad (\text{A21}) \end{aligned}$$

which is the expression derived by Li *et al.*

## APPENDIX B: FLUX-SURFACE AVERAGE OF THE GKP EQUATION

In the local toroidal system  $\{r, \theta, \phi\}$ , the surface average of  $F$  is

$$\langle F \rangle_S \equiv \frac{1}{A} \int_0^{2\pi} d\phi \int_0^{2\pi} d\theta F(r, \theta, \phi) \mathcal{J}(r, \theta), \quad (\text{B1})$$

where  $\mathcal{J} = [\nabla r \cdot (\nabla \theta \times \nabla \phi)]^{-1} = r(R_0 + r \cos \theta)$  is the Jacobian of the transformation and  $A \equiv \int_0^{2\pi} d\phi \int_0^{2\pi} d\theta \mathcal{J}(r, \theta) = 4\pi^2 r R_0$  is the area of the magnetic surface. Then we note that

$$\begin{aligned} \langle \exp(im\theta + in\phi) \rangle_S &= \delta(n) \delta(m) + \frac{r}{2R_0} \delta(n) [\delta(m+1) + \delta(m-1)], \quad (\text{B2}) \end{aligned}$$

where the second term on the right-hand side is a finite-toroidicity correction. The surface average of  $\langle \tilde{\Phi} \rangle_{\text{part}}$  involves terms of the form  $\langle J_k(F) J_l(G) J_m(H) \exp(im\theta) \rangle_{\text{part}}$

$+in\phi\rangle_{\text{part}}$ , where, in general,  $F=F(r, \theta, \phi)$ ,  $G=G(r, \theta, \phi)$ ,  $H=H(r, \theta, \phi)$ , and  $k, l, m$  are integers. Without loss of generality, we can write

$$F(r, \theta, \phi) = \bar{F}(1 - f), \tag{B3}$$

where  $\bar{F}(r) \equiv \langle F \rangle_S$  is a flux surface quantity, and  $f(r, \theta, \phi) \equiv 1 - F(r, \theta, \phi)/\bar{F}$ . Similarly one may write  $G = \bar{G}(1 - g)$

and  $H = \bar{H}(1 - h)$ ; by construction, we note that  $\langle f \rangle_S = \langle g \rangle_S = \langle h \rangle_S = 0$ . Typically the ratio  $|f/\bar{F}|$  is of the order of the inverse aspect ratio. Using a Taylor expansion

$$J_k(F) = J_k(\bar{F}) + \frac{f}{2} [J_{k+1}(\bar{F}) - J_{k-1}(\bar{F})] + \dots \tag{B4}$$

and similarly for  $J_l(G)$  and  $J_m(H)$ , we obtain (neglecting higher-order corrections)

$$\begin{aligned} &\langle J_k(F) J_l(G) J_m(H) \exp(im\theta + in\phi) \rangle_S \\ &= J_k(\bar{F}) J_l(\bar{G}) J_m(\bar{H}) \langle \exp(im\theta + in\phi) \rangle_S + \frac{1}{2} J_k(\bar{F}) J_l(\bar{G}) [J_{m+1}(\bar{H}) - J_{m-1}(\bar{H})] \langle h(r, \theta, \phi) \exp(im\theta + in\phi) \rangle_S \\ &\quad + \frac{1}{2} J_k(\bar{F}) J_m(\bar{H}) [J_{l+1}(\bar{G}) - J_{l-1}(\bar{G})] \langle g(r, \theta, \phi) \exp(im\theta + in\phi) \rangle_S \\ &\quad + \frac{1}{2} J_l(\bar{G}) J_m(\bar{H}) [J_{k+1}(\bar{F}) - J_{k-1}(\bar{F})] \langle f(r, \theta, \phi) \exp(im\theta + in\phi) \rangle_S + \dots \end{aligned} \tag{B5}$$

Then, to leading order, the flux-surface average of  $\langle \tilde{\Phi} \rangle_{\text{part}}$  becomes

$$\begin{aligned} \langle \langle \tilde{\Phi} \rangle_{\text{part}} \rangle_S &= \sum_{l=1}^{\infty} \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \Phi_{lmn} \left\{ J_m(\beta_{ml}r) - \sum_{k=-\infty}^{\infty} (-1)^k J_k[\beta_{ml}\langle \rho_i \rangle_S V_{\perp}] J_k[\langle k_t \rho_i \rangle_S V_{\perp}] J_{m+k}(\beta_{ml}r) J_0[\langle \hat{k} \rho_i \rangle_S V_{\perp}] \right. \\ &\quad \left. + \frac{\beta_{ml}}{4} \langle \rho_i \rangle_S V_{\perp} \sum_{k=-\infty}^{\infty} (-1)^k J_k[\beta_{ml}\langle \rho_i \rangle_S V_{\perp}] J_k[\langle k_t \rho_i \rangle_S V_{\perp}] [J_{m+k+1}(\beta_{ml}r) - J_{m+k-1}(\beta_{ml}r)] \right. \\ &\quad \left. \times [J_1(y_+ V_{\perp}) - J_1(y_- V_{\perp})] + \dots \right\} \langle \exp(im\theta + in\phi) \rangle_S, \end{aligned} \tag{B6}$$

where  $y_{\pm} \equiv [(m \pm 1)/r + n/R_0] \langle \rho_i \rangle_S$ . Here  $\langle \rho_i \rangle_S$  is the surface-average of the ion thermal gyroradius  $\rho_i \equiv v_{\text{th}i}/\omega_c$ . Since the toroidal wave number  $k_t \propto 1/R$ , we note that  $\langle k_t \rho_i \rangle_S \neq k_t \langle \rho_i \rangle_S$ . Equation (B6) can be simplified by using the following properties<sup>15</sup> of the Bessel functions  $J_N(x) \sim (x/2)^N/\Gamma(N+1)$  for  $|x| \rightarrow 0$ , and  $J_{-N}(x) = (-1)^N J_N(x)$ ; whereas the integral representation (A16) shows that  $J_k(0) = \delta(k)$ . We obtain

$$\begin{aligned} \langle \langle \tilde{\Phi} \rangle_{\text{part}} \rangle_S &= \sum_{l=1}^{\infty} \Phi_{l00} \left[ J_0(\beta_{0l}r) - J_0(\beta_{0l}\langle \rho_i \rangle_S V_{\perp}) J_0(\beta_{0l}r) \right. \\ &\quad \left. + \frac{\beta_{0l}}{2} \frac{\bar{\rho}^2/r}{\Gamma(2)} V_{\perp}^2 J_1(\beta_{0l}r) J_0(\beta_{0l}r \langle \rho_i \rangle_S V_{\perp}) + \dots \right]. \end{aligned} \tag{B7}$$

Substituting Eq. (B7) in the GKP equation (3) we get

$$\begin{aligned} &\sum_{l=1}^{\infty} \Phi_{l00} \left[ J_0(\beta_{0l}r) - J_0(\beta_{0l}r) \right. \\ &\quad \left. \times \left[ \int_0^{\infty} V_{\perp} \exp(-V_{\perp}^2/2) J_0(\beta_{0l}\langle \rho_i \rangle_S V_{\perp}) dV_{\perp} \right] \right. \\ &\quad \left. + \frac{\beta_{0l}}{2} \frac{\langle \rho_i \rangle_S^2/r}{\Gamma(2)} J_1(\beta_{0l}r) \right] \end{aligned}$$

$$\begin{aligned} &\times \left[ \int_0^{\infty} V_{\perp}^3 \exp(-V_{\perp}^2/2) J_0(\beta_{0l}\langle \rho_i \rangle_S V_{\perp}) dV_{\perp} \right] + \dots \Big] \\ &= \frac{T_{i0}}{en_0} \langle \bar{n}_i - n_e^{(\text{NA})} \rangle_S. \end{aligned} \tag{B8}$$

The first integral on the left-hand side of Eq. (B8) is of the form<sup>14</sup>

$$\begin{aligned} \mathcal{L}_{\nu}(\alpha, \beta) &= \int_0^{\infty} x^{\nu+1} \exp(-\alpha x^2) J_{\nu}(\beta x) dx \\ &= \frac{\beta^{\nu}}{(2\alpha)^{\nu+1}} \exp\left(-\frac{\beta^2}{4\alpha}\right). \end{aligned} \tag{B9}$$

Noting that

$$\begin{aligned} &\int_0^{\infty} x^3 \exp(-\alpha x^2) J_0(\beta x) dx \\ &= -\frac{\partial \mathcal{L}_0(\alpha, \beta)}{\partial \alpha} = \frac{1}{2\alpha^2} \left( 1 - \frac{\beta^2}{4\alpha} \right) \exp\left(-\frac{\beta^2}{4\alpha}\right). \end{aligned} \tag{B10}$$

we obtain an equation governing the sheared-flow modes in toroidal geometry

$$\sum_{l=1}^{\infty} \Phi_{l00} \left\{ J_0(\beta_{0l}r) [1 - \exp(-C_l^2/2)] + \frac{\langle \rho_i \rangle_S / r}{\Gamma(2)} J_1(\beta_{0l}r) C_l \left( 1 - \frac{C_l^2}{2} \right) \exp(-C_l^2/2) \right\} = \mathcal{D}(r), \quad (\text{B11})$$

where  $C_l \equiv \beta_{0l} \langle \rho_i \rangle_S$  and  $\mathcal{D}(r) \equiv T_{i0} [\langle \bar{n}_i \rangle_S - \langle n_e^{(\text{NA})} \rangle_S] / (en_0)$ .

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